EQUILIBRIUM OF COMPRESSION-ONLY STRUCTURES MADE OF CONVEX POLYHEDRA

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#### LET'S TALK ABOUT...

1. Compression Structures

Basic definition and some examples.

2. Equilibrium Analysis Reasoning about equilibrium and forces. 3. Assemblies Made of Convex Polyhedra

Counterintuitive  $\frac{y}{y}$  structures made z possible.

Perspectivez

# Compression Structures

What are they and why they matter

XYZ

Figh

### **COMPRESSION STRUCTURE**

Compressive loads applied along the structure.
 The compression load applied to the cross section of structure produces stress.
 Best when using rigid materials.

### Alcántara Bridge Extremadura, Spain

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and the state of the sector of the sector of the

124.

By Dantla from de.wikipedia - Own work, GFDL, https://commons.wikimedia.org/w/index.php?curid=455958

### Igloo at Night, Vermillion Lakes, Banff National Park, Alber Bridge

By Jochi, https://wall.alphacoders.com/big.php?i=437732

### Droneport Prototype Venice, Italy

Block Research Group (BRG), © Nigel Young and The Norman Foster Foundation https://block.arch.ethz.ch/brg/project/venice-biennale-2016\_droneport

### THE RED LINE PROJECT

Block Research Group (BRG), © Foster + Partners https://block.arch.ethz.ch/brg/project/venice-biennale-2016\_droneport



### Sagrada Família Barcelona, Spain

HTTPS://WALLPAPERCAVE.COM/W/WP3766514





### PRINGLES RING

http://www.blazenfluff.com/one-pringle-to-rule-them-all-how-to-make-a-stacked-ring-of-pringles/5672



https://www.pbs.org/wgbh/nova/physics/arch-physics.html

# 2. Equilibrium Analysis

XYZ

righ

A bit of formality

**Emily Whiting** R. K. Livesley Me Cambridge MIT Purdue 1978 2009 2019 1992 ... Please, don't move! Even in 3D! Let's relax No forces? Then no possible .

Livesley, R. K. "Limit Analysis of Structures Formed from Rigid Blocks." International Journal for Numerical Methods in Engineering 12, no. 12 (1978): 1853–71. Livesley, R. K. "A Computational Model for the Limit Analysis of Three-Dimensional Masonry Structures." Meccanica 27, no. 3 (1992): 161–72. Whiting, Emily, John Ochsendorf, Frédo Durand, "Procedural Modeling of Structurally-Sound Masonry Buildings." In ACM Transactions on Graphics (TOG), 28:112. ACM, 2009.

Forward Statics Problem

## **1. DENSITY** It is uniform for all blocks

# 2. FRICTION

It exists between blocks

# 3. GRAVITY It pulls everything down

Taht

Interface Polygons & Contact Forces

 $f^{i+3}$ 

fi

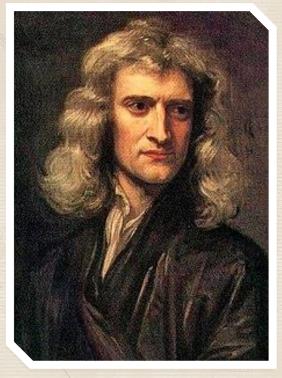
 $f^{i+2}$ 

 $f^{i+1}$ 

 $f_n^i$ 

 $f_u^i$ 

 $f_v^i$ 

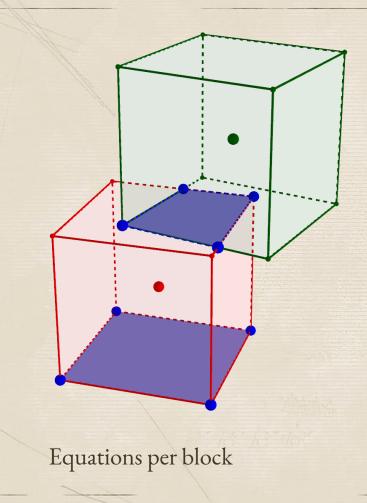


By After Godfrey Kneller - http://www.newton.cam.ac.uk/art/portrait.html, Public Domain https://commons.wikimedia.org/w/index.php?curid=37337

### NEWTON'S FIRST LAW OF MOTION

"Every body persists in its state of being at rest or of moving uniformly straight forward, except insofar as it is compelled to change its state by force impressed."

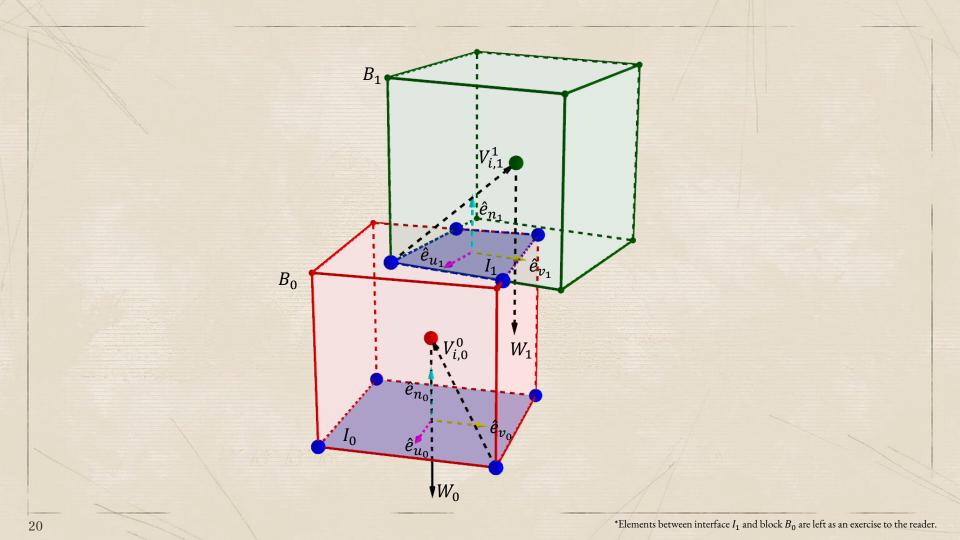
 $\sum F = 0$ 

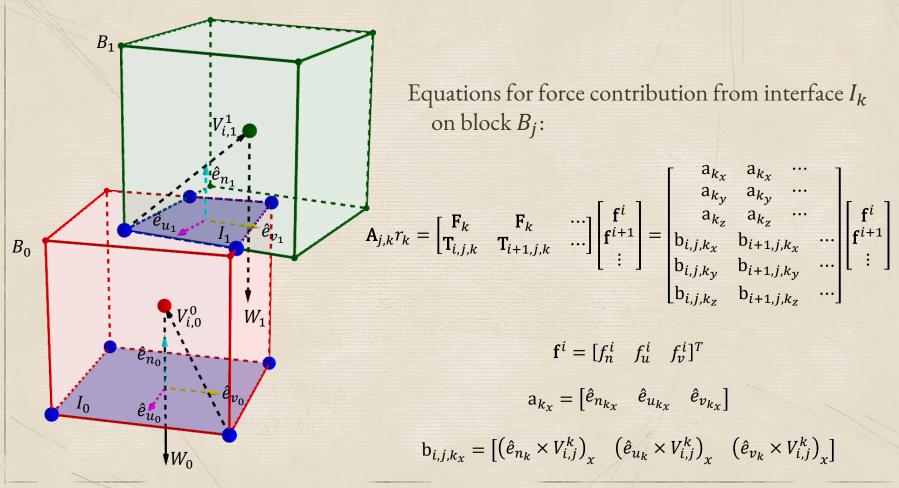


Net force and net torque per block:  $\sum F = 0$  and  $\sum T = 0$ 

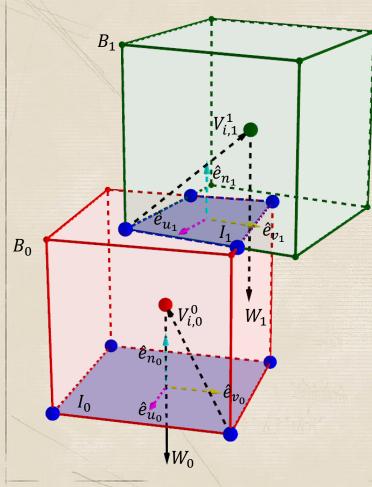
Six equations per block:  $\sum F_x = 0 \quad \sum F_y = 0 \quad \sum F_z = 0$   $\sum T_x = 0 \quad \sum T_y = 0 \quad \sum T_z = 0$ 

Each interface contributes with forces and torques on its incident blocks.Interactions with the ground are considered as interfaces too.





\*Flip  $a_k$  when  $\hat{e}_{n_k}$  faces an opposite direction with respective of the centroid of a block.



Equation for all interactions between interfaces and blocks:

$$\begin{array}{ccc} \mathbf{A}_{0,0} & \mathbf{A}_{0,1} \\ & \ddots \\ & \mathbf{A}_{n-1,n-1} & \mathbf{A}_{n-1,n} \end{array} \right] \begin{bmatrix} \mathbf{r}_0 \\ \vdots \\ \mathbf{r}_n \end{bmatrix} + \begin{bmatrix} \mathbf{w}_0 \\ \vdots \\ \mathbf{w}_{n-1} \end{bmatrix} = 0$$

 $\mathbf{A}_{eq} \cdot \mathbf{f} + \mathbf{w} = 0$ 

A<sub>j,k</sub>: Submatrix of coefficients for net contributions from interface k acting on block j.
w<sub>j</sub>: 6 × 1 vector containing the 3D weight and net torque for block j.

 $r_k$ : Unknown force vectors for vertices *i* on interface *k*.

# **Compression Constraint:** $f_n^i \ge 0, \forall i \in \text{interface vertices}$

**Linearized Friction Constraints:**  $|f_u^i|, |f_v^i| \le \mu f_n^i, \forall i \in \text{interface vertices}$ 

 $\mathbf{A}_{fr} \cdot \mathbf{f} \leq 0$ 

Force Constraints

 $f_v^i$ 

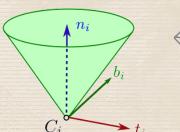
fui

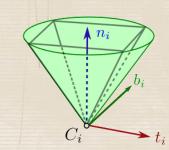
 $f^{i+3}$ 

 $f^{i+2}$ 

fi+1

 $f_n^i$ 





 $|f_u^i|, |f_v^i| \le \mu f_n^i, \forall i \in \text{interface vertices}$ 

 $n_i$ 

 $|f_u^i|, |f_v^i| \le \frac{\mu f_n^i}{\sqrt{2}}, \forall i \text{ (conservative)}$ 

8-sided pyramids are also possible (requires more calculations)

Why linearized friction constraints?

mg

C

fext

### **REMEMBER LIVESLEY?**

Structure in equilibrium if a force solution **f** exists that satisfies:

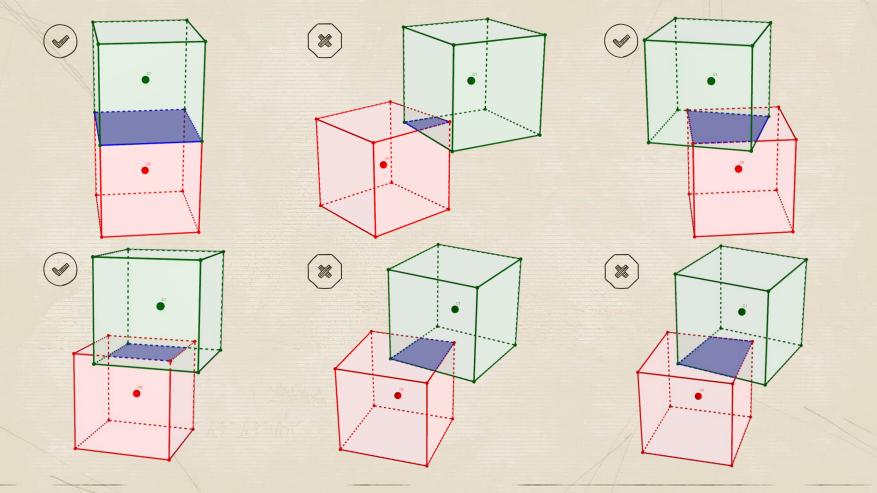
XYN

height, h.

ground

POFSPEC

$$\begin{aligned} \mathbf{A}_{eq} \cdot \mathbf{f} + \mathbf{w} &= 0\\ \mathbf{A}_{fr} \cdot \mathbf{f} &\leq 0\\ f_n^i &\geq 0, \forall i \in \text{interface vertices} \end{aligned}$$



GLUE

× 5 N

height, h,

Z

Stound

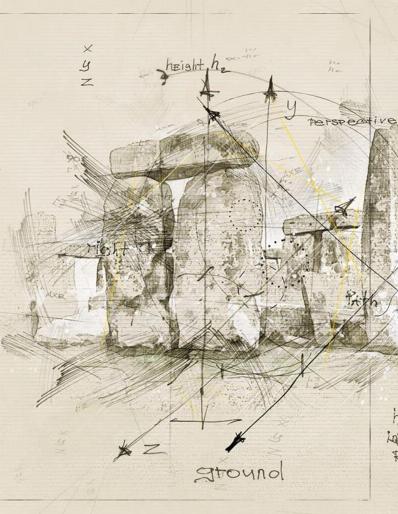
Perspective

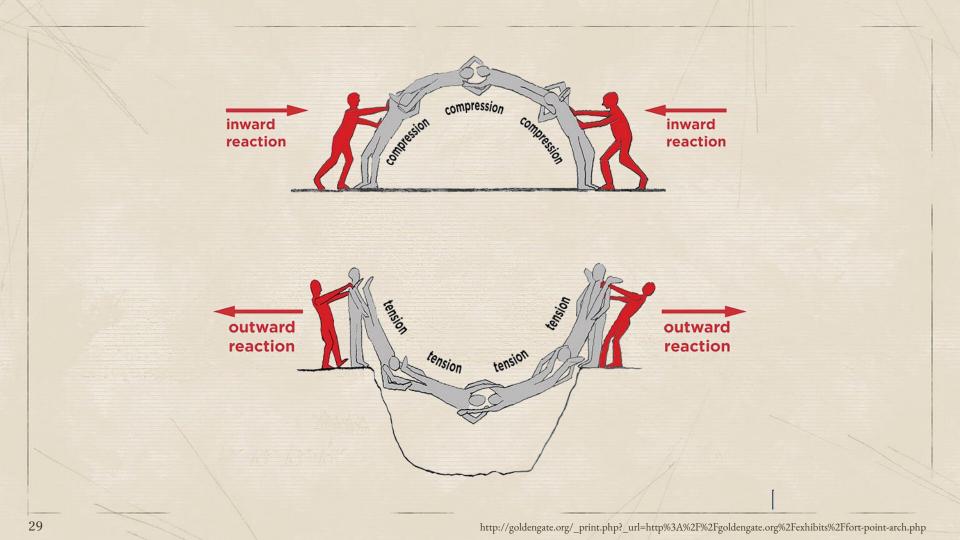
Use glue!

Decompose  $f_n^i$  into compression and tension components...

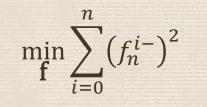
$$f_n^i = f_n^{i+} - f_n^{i-}$$

$$f_n^{i+}, f_n^{i-} \ge 0$$

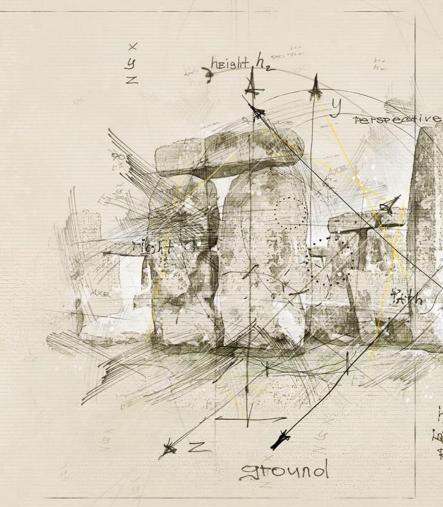




#### ... but penalize tensions:



 $\begin{aligned} \mathbf{A}_{eq} \cdot \mathbf{f} + \mathbf{w} &= 0\\ \mathbf{A}_{fr} \cdot \mathbf{f} &\leq 0\\ f_n^{i+}, f_n^{i-} &\geq 0, \forall i \end{aligned}$ 

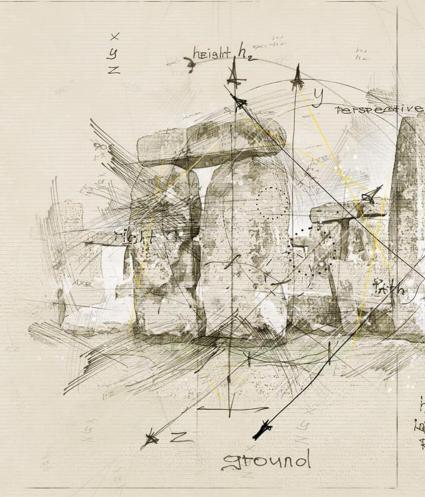


\*Update  $\mathbf{A}_{eq}$ ,  $\mathbf{A}_{fr}$  and  $\mathbf{f}$  for handling compression and tension components.

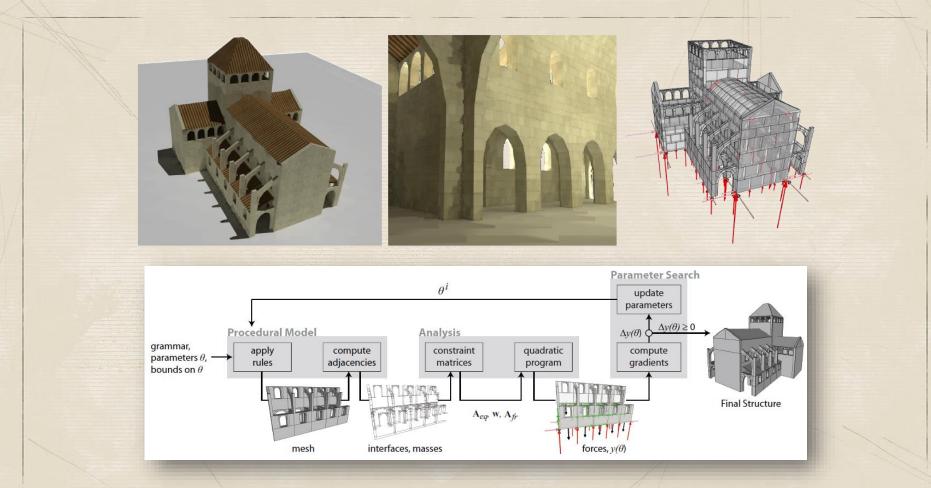
#### Quadratic program for all forces:

 $g(\mathbf{f}) = \min_{\mathbf{f}} \frac{1}{2} \mathbf{f}^T \mathbf{H} \mathbf{f}$ 

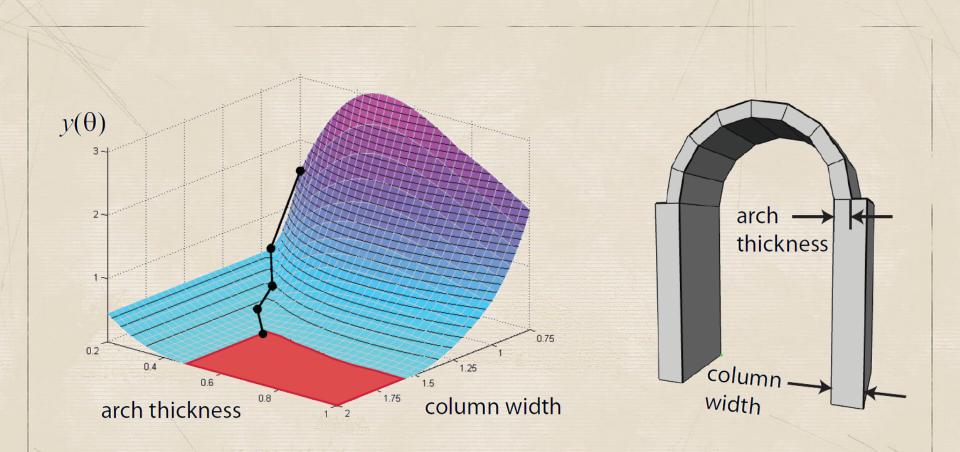
$$\mathbf{A}_{eq} \cdot \mathbf{f} + \mathbf{w} = 0$$
$$\mathbf{A}_{fr} \cdot \mathbf{f} \le 0$$
$$f_n^{i+}, f_n^{i-} \ge 0, \forall i$$



\*Solution exists if H is positive semidefinite.



Whiting, Emily, John Ochsendorf, Frédo Durand, Emily Whiting, John Ochsendorf, and Frédo Durand. "Procedural Modeling of Structurally-Sound Masonry Buildings." In ACM Transactions on Graphics (TOG), 28:112. ACM, 2009.



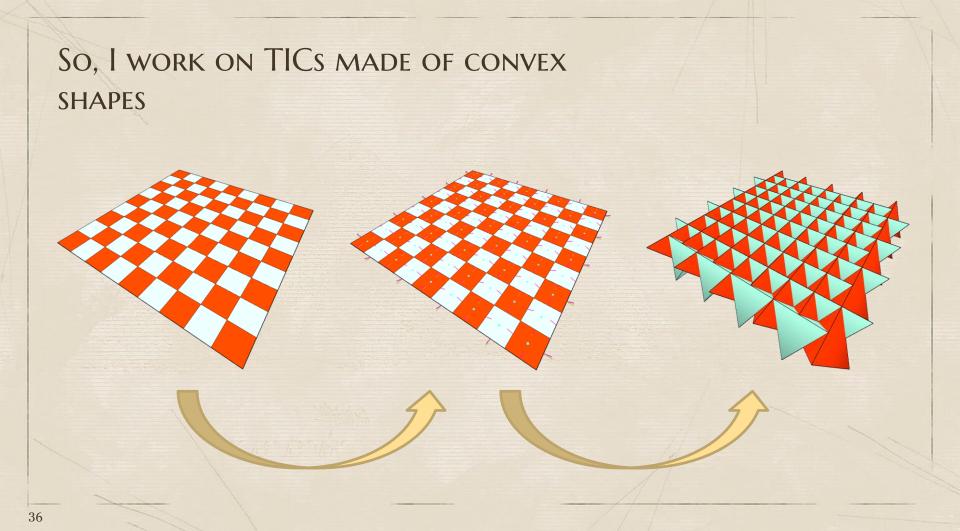
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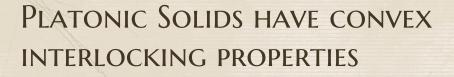


# 3. Assemblies made of Convex Polyhedra

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Structures made the hard way







<sup>66</sup> It's TIC time!

# BE GENTLE WITH THOSE ANIMALS!

# **DARE YOU!**

Take 9 tetrahedra and put them together as shown. Then, lift them up and keep the piece in the middle on interlocking (5 seconds).

## BIG PROBLEM: FUNCTIONAL 3D TICS

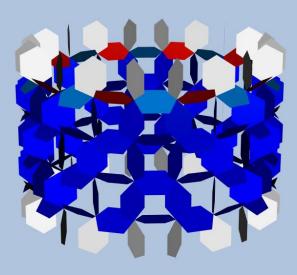
 $f(\psi)$ 





Radius: 1 Pieces per ring: 20

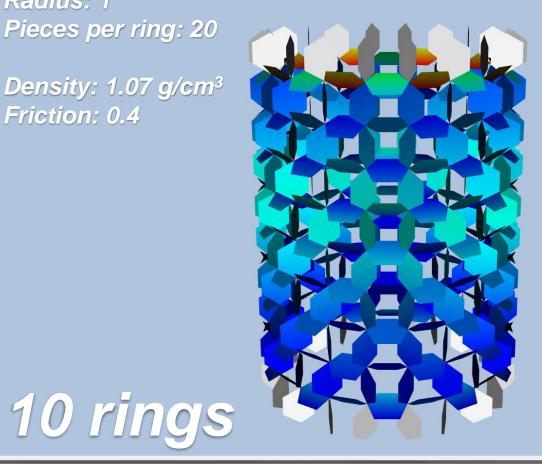
#### Density: 1.07 g/cm<sup>3</sup> Friction: 0.4



Tension 0.0150 0.0120 0,00898 0,00599 0.00299 -1.00*ə-0*8



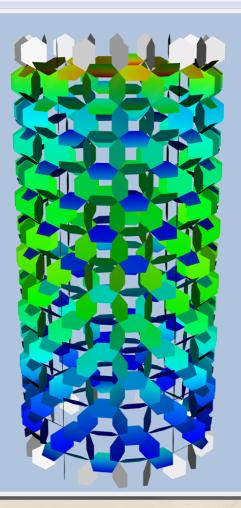
Radius: 1 Pieces per ring: 20

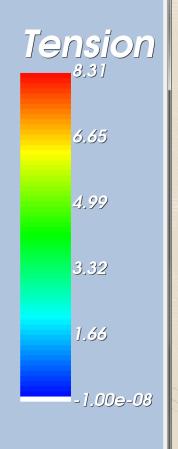




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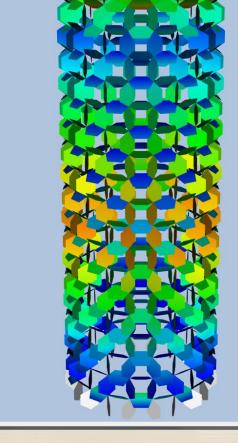






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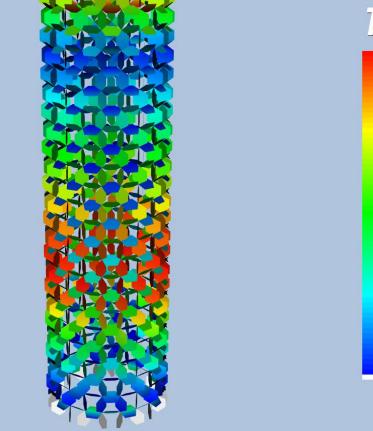
Density: 1.07 g/cm<sup>3</sup> Friction: 0.4

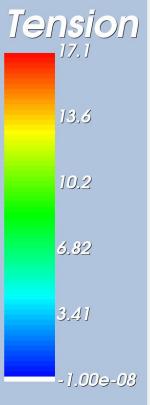




Radius: 1 Pieces per ring: 20

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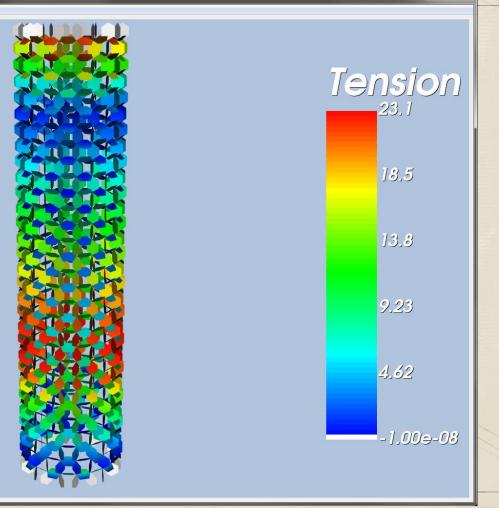




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*Radius: 1 Pieces per ring: 20* 

#### Density: 1.07 g/cm<sup>3</sup> Friction: 0.4

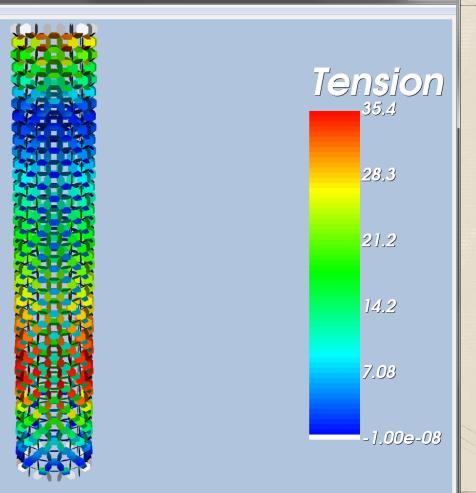


Radius: 1 Pieces per ring: 20



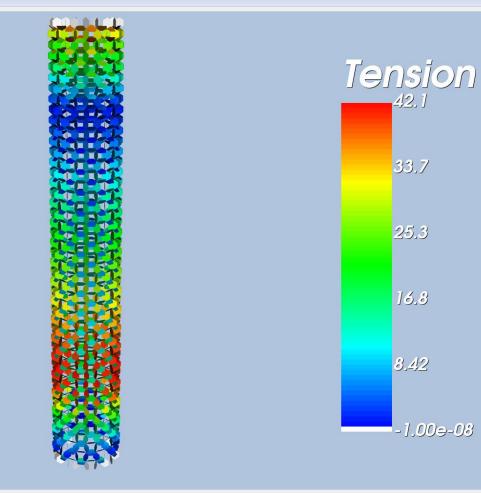


Radius: 1 Pieces per ring: 20

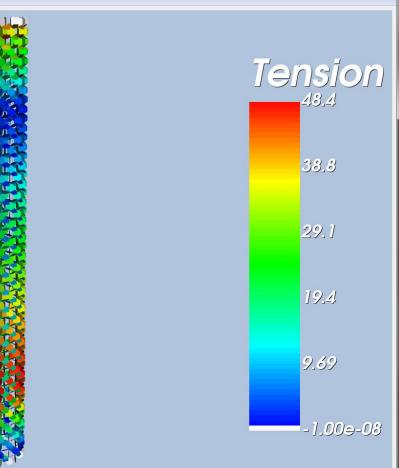




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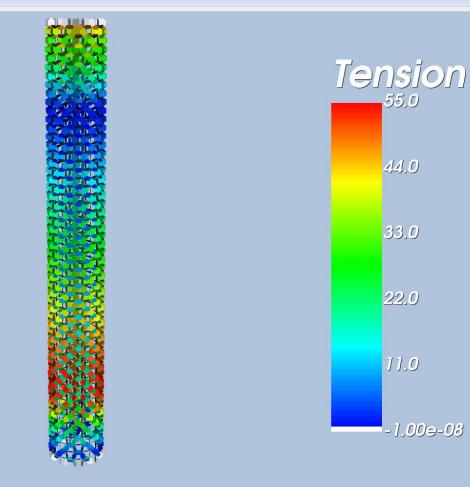






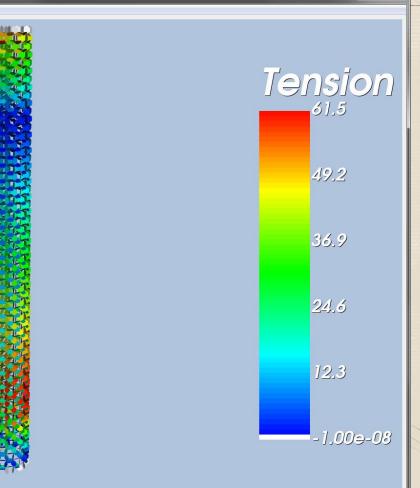
#### Density: 1.07 g/cm<sup>3</sup> Friction: 0.4

55 rings

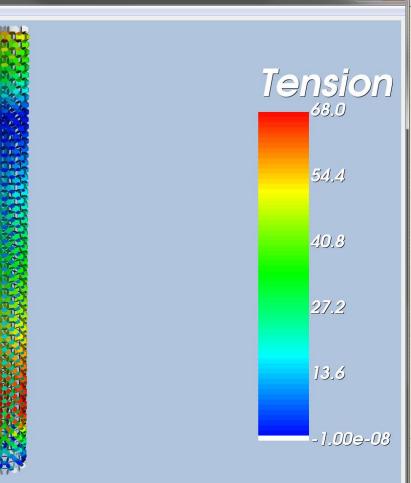


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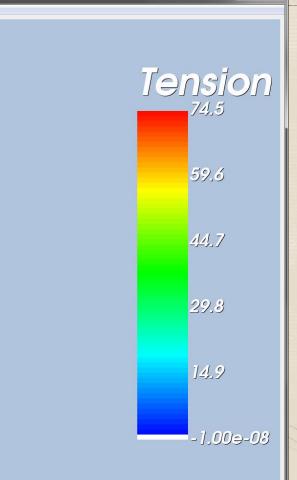






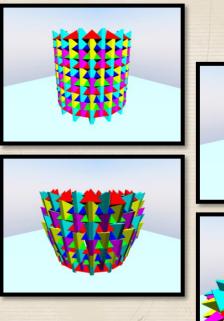


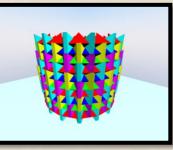


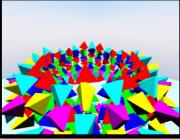


## WHAT'S WRONG WITH SIMULATIONS?

Yes/no answer
What should we simulate?
Makes sense?







### QUESTIONS

How do we generate pieces different than antiprisms? How about Archimedean and Catalan Solids? ♦ Do TICs guarantee stability? Does the piece shape affect stability? ♦ Does it work using free form geometric domains (e.g., Stanford Bunny)?

# Episode 2 **General Mid-Section Evolution for TIC** Generation

November 20<sup>th</sup>, 2019

# **THANKS!** Any questions? You can find me at: ♦ @andresbeja87 ♦ abejara@purdue.edu Office #19

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### CREDITS

Special thanks to all the people who made and released these awesome resources for free:

 Presentation template and backgrounds by <u>SlidesCarnival</u>
 Photographs by <u>Unsplash</u>

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